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## ⑫ 公表特許公報 (A)

昭56—500666

⑤ Int. Cl.<sup>3</sup>

F 41 G 3/26

識別記号

庁内整理番号

6935—2C

⑭ 公表 昭和56年(1981)5月14日

部門(区分) 5(3)

審査請求 未請求

(全 6 頁)

## ⑭ 兵器効果シミュレータ

① 特 願 昭55—501066  
 ② 出 願 昭55(1980)5月22日  
 翻訳文提出日 昭56(1981)1月26日  
 ③ 国際出願 PCT/GB80/00092  
 ④ 国際公開番号 WO 80/02741  
 ⑤ 国際公開日 昭55(1980)12月11日  
 優先権主張 ⑥ 1979年5月25日 ⑦ イギリス(GB)  
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 ⑫ 指 定 国 DE, GB, JP, SE, US

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## 請 求 の 範 囲

1. 兵器の模擬発射期間中に電磁波ビームを照射するように構成された照射器と、入射した前記電磁波ビームを輸出するように構成された輸出器とを備える兵器効果シミュレータであつて、前記照射器は前記各発射ごとに少くとも1つの電磁波パーストを発生するように構成され、その電磁波パーストの持続時間は予め定められ、かつ前記電磁波パーストは所定の周波数で変調され、前記輸出器は、前記所定の周波数に対して高調波関係にある周波数に同調され、かつ前記持続時間に依存する通過帯域を有する周波数選択要素を含むことを特徴とする兵器効果シミュレータ。
2. 特許請求の範囲の第1項に記載のシミュレータであつて、前記変調はパルス変調であることを特徴とするシミュレータ。
3. 特許請求の範囲の第1項に記載のシミュレータであつて、前記変調は持続波変調であることを特徴とするシミュレータ。
4. 特許請求の範囲の第1項に記載のシミュレータであつて、前記周波数選択要素は前記所定の周波数に同調させられることを特徴とするシミュレータ。
5. 特許請求の範囲の第1項に記載のシミュレータであつて、前記通過帯域は前記持続時間の逆数の2倍にほぼ等しいことを特徴とするシミュレータ。

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6. 特許請求の範囲の第1項に記載のシミュレータであつて、前記輸出器は1つの増幅器へ並列に結合される複数の感光素子を有することを特徴とするシミュレータ。

#### 技術的背景

本発明は兵器効果シミュレータに関するものである。

#### 背景技術

訓練のために、兵器を模擬操作している間に電磁波（典型的にはレーザ）のビームを用いることが知られている。1つの種類の装置においては（英国特許明細書第1228143号、第1228144号、第1439612号、第1451192号）、適切であれば見越しのような要素を調整することにより、弾（砲弾または銃丸）の「発射」時に兵器（たとえば小銃）が向けられている向きと同じ向きに電磁波ビームが向けられる。別の種類の装置においては（英国特許明細書第1300941号および第1300942号）、弾（たとえばミサイル）が実際に発射された時にたどるであろう弾道に連続して交差する向きに電磁波ビームが照射される。いずれの装置においても、標的附近に達した弾により占められる空間中の点に電磁波ビームが向けられることになる。

それらの装置は、電磁波ビームを発生し、必要がある場合にはビームの向きを定めるための、照射器として一般に知られている装置と、標的に入射した電磁波を検出するための、検出器として知られている、別の装置とを含む。この検出器は標的自体にとりつけることもでき

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時間は予め定められ、かつ前記電磁波パーストは所定の周波数で変調され、前記検出器は、前記所定の周波数に同調され、かつ前記持続時間に依存する通過帯域を有する周波数選択要素を含む兵器効果シミュレータが得られる。

電磁波は、個々のパルスを一々に検出する（パルス変調の場合に）のではなくて、全体のパーストとその変調（変調は、たとえば、パルス変調または持続波変調にできる）の検出により検出される。

周波数選択器の通過帯域は前記所定の持続時間の逆数の2倍にほぼ等しくできる。この持続時間を比較的長くすることにより（たとえば1ミリ秒）、通過帯域を非常に狭く（わずかに2kHz）でき、それにより数個のホトセルを並列に結合できる程度まで、ノイズをかなり減少させることができる。

更に、与えられたB/N比で放射せねばならないピーク電力は大膽に減少せられ、そのために、たとえばピーク出力が低く、平均出力が高い装置、たとえば二重ヘテロ構造レーザおよび小型の発光ダイオードを用いることができる。

#### 図面の簡単な説明

添付図面を参照して実施例を用い本発明の兵器効果シミュレータを説明する。ここで、第1図は射撃訓練兵と標的兵を示す略図、第2図は照射器の一実施例のブロッ

ク図、第3図は照射器の別の実施例のブロック図、第4図は検出器の回路図、第5、6図はそれぞれパルス変調と持続波変調を示すダイミング波形図である。

それらの装置においては、幅が非常に狭く、かつピーク電力が比較的高いパルスの形で電磁波を照射するように電磁波照射器が構成されている。したがって、各電磁波パルスを個々に検出するように検出器（増幅器に結合されているホトセル）が構成されている。パルスは衝撃性のものであるから、検出器に用いられている増幅器の帯域幅は比較的広くしてパルスを確実に検出できるようにせねばならない。しかし、そうすると、許容B/N比を維持すべきものとすれば、増幅器に接続できるホトセルの数が1個に制限される。実際には、標的を中心とする任意の方向からの電磁波を検出するために標的に少くとも4個のホトセルを設ける必要があり、かつ各ホトセルにはそれぞれ高選択度、高安定および広帯域（したがって高価な）増幅器を必要とする。

#### 発明の開示

本発明の1つの面に従つて、兵器の模擬発射期間中に電磁波ビームを照射するように構成された照射器と、入射した前記電磁波ビームを検出するように構成された検出器とを備える兵器効果シミュレータであつて、前記照射器は前記各発射ごとに少くとも1つの電磁波パーストを発生するように構成され、その電磁波パーストの持続

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性

まず第1図を参照して、訓練中の射撃兵10が標的兵14に小銃12のねらいをつけている。小銃12には空包が装填されており、かつレーザ照射器16がとりつけられている。標的兵14の肩部には2個の検出器18がとりつけられ、ベルト22には4個の検出器20がとりつけられる。全ての検出器18、20はベルト22にとりつけられている制御器および発煙器24へ接続される。

射撃兵10が小銃12の引金を引くと空包が破裂して音と光が生ずる。それと同時にレーザ照射器16が自動的に動作させられて、電磁波ビームを小銃12の照準の向きに照射する。小銃が標的兵14に正確に照準されておれば電磁波ビームが検出器18と20の少くとも一方に入射して、信号が制御器および発煙器24へ送られる。そうすると発煙器24から煙が出て標的兵14に弾が当たったことを示す。標的兵14も小銃を持つているものとする、弾が当たった時にその小銃の発射を禁止するようにその小銃は制御器24へ結合される。

次に、照射器16と制御器24の構成と動作を第2～

6図を参照して詳しく説明する。

まず第3図を参照して、小銃12の発射は発射センサ30により検知される。この発射センサ30は、たとえば、小銃12の発射音を検知するマイクロホンおよび増幅器で構成することもできれば、空包が発射された時に小銃の銃身中に生ずる背圧により動作させられる圧カスイッチで構成することもできる。発射センサ30は単安定回路32をトリガし、そのために単安定回路32は持続時間が1ミリ秒のパルスを出給して無安定回路34を動作させる。この無安定回路34は繰り返し周波数が170 KHzのパルスをひ化カリウム二重ヘテロ構造レーザ36へ与えて、繰り返し周波数が170 KHzで、持続時間が1ミリ秒の赤外線パルスを発生させる。このレーザ36の前方に置かれているレンズにより赤外線はビーム状に収束される。

第2図に示されている照射器においては、小銃12の発射ごとに赤外線のパルスのバーストが1つだけ照射される。しかし、希望によつては第3図に示す回路を用いて、各発射ごとにいくつかのバーストを照射させることができる。

次に第3図を参照する。発射センサ30は単安定回路40と第2の無安定回路42を介して無安定回路34へ接続される。単安定回路40はトリガされると持続時間が9ミリ秒のパルスを無安定回路42へ与える。そうするとこの無安定回路は500 Hzの周波数で動作する。

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増幅器18, 20(すなわち、感光素子50のいずれか)に入射した赤外線パルスのために、それに対応する電気パルスがコンデンサ54とトランス56を介して増幅器58へ与えられる。この増幅器で増幅された170 KHzのパルスの1ミリ秒バーストはフィルタ60により処理されてから比較器74へ与えられる。この比較器74は、処理された信号の振幅があるしきい値電圧をこえた時に、発射器を動作させる。

第5図は典型的な赤外線パルスバーストのタイミング波形図で、各パルスバーストは、1ミリ秒期間中発生される、パルス間隔が6マイクロ秒で、パルス幅が350ナノ秒のパルスで構成される。この波形に等価な周波数領域を第5図bに示す。この周波数領域は0 Hzが中心である主ローブと、170 KHzの整数倍が中心である副ローブとを有する。各ローブは2 KHzの周波数範囲を囲む。

フィルタ60の作用は+170 KHzと-170 KHzを中心とするローブを選択することである。+170 KHzと-170 KHzの符号の+と-は両方の信号の位相が互いに逆であることを示すものである。フィルタ60の通過帯域2 KHzはパルスバーストの周波数スペクトラム中の2 KHz範囲に関連するもので、この範囲は各バーストの持続時間1ミリ秒により決定される。したがって、フィルタ60の動作は、あるバーストが持続されている間のそのバーストに含まれている全てのパル

そのために無安定回路34は5周期だけ動作させられる。各周期の持続時間は1ミリ秒で、周期と間期の間は1ミリ秒だけ隔てられる。無安定回路34の動作によりレーザ36は繰り返し周波数が170 KHzの赤外線パルスバーストを5つ発射する。

次に第4図を参照する。増幅器18, 20は、相互間およびチヨーク52と並列に接続される無バイアス感光シリコン素子50で扱われている。チヨーク52は周波数により感光素子50中に生じた電荷のための直流流れ経路を形成し、それによりそれらの電荷が蓄積されて感光素子50を飽和させることを防ぐ。チヨーク52により影響を受けない高周波信号はコンデンサ54を介して結合トランス56の1次巻線へ結合される。結合トランス56の1次巻線と2次巻線の巻数比は8/N比を最適にするように選択され、2次巻線の端子間に現われた信号が通常の低雑音増幅器58へ与えられる。この増幅器58にはその高周波応答を制限するための小容量帰還コンデンサが設けられる。

増幅器58の出力端子は3段帯域フィルタ60へ結合される。このフィルタの各段は増幅器62, 64, 64と、中心周波数が170 KHzで、通過帯域幅が2 KHzである並列共振帯域通過LCフィルタ68, 70, 72でそれぞれ構成される。処理された信号は比較器74へ与えられる。この比較器はダイオード検波-復調器76を介して発射器を制御する。

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スを増分することであると考えられることができるから、各パルスのエネルギーはそのバーストに含まれている他の全てのパルスのエネルギーに加え合わされる。したがって、前記した比較的安価な二重ヘテロ構造素子のような、ピーク出力は比較的低いが、平均出力が比較的高いレーザ装置を照射器16に用いることができる。そのために、温度変化に対する照射器の動作が安定になるとともに、小型で低電圧の駆動トランジスタをレーザ装置に用いることができるという利点が得られる。フィルタ60の帯域幅が2 KHzと比較的狭いから、感光素子50の出力信号中に占めるノイズの割合が大いに低下し、そのためにピーク出力の低いレーザ装置を使用することが容易となるとともに、第4図に示すように、何個かのホトセルを1つの増幅器58へ並列に接続できることになる。

170 KHzに同調している帯域フィルタ60を低域フィルタの代りに用いて、第5図bに示されている、0 Hzを中心とする主ローブを検出することにより、周波数の急変、またはこの装置の設置および設定中に受けることがある人工光により発生させられるスプリアス信号を避けることができる。帯域フィルタ60は170 KHz自体でなく、その高調波(たとえば340 KHz)に同調させることができる。更に、希望の帯域通過周波数に感光素子50の自己容量に組合わされて共振するようにチヨーク52のインダクタンスを選択することにより

結合トランス56より前に周波数選択を行うことができる。

照射器16により照射される電磁波はパルス変調の代りに、第6図に示されているような持続波変調とすることもできる。この場合には、第2, 3図に示されている無安定回路34の代りに適当な正弦波発振器が用いられる。第6図はこの種の波変調の周波数スペクトラムを示すものである。この場合には、帯域フィルタ60は電磁波の1ミリ秒パーストの変調周波数(170 KHz)に同調させられる。ストライプド・ジオメトリ型レーザ小型の発光ダイオードがとくに適当である持続波変調の場合には、パルス変調の場合よりかなり大きな(半分まで)変調電力をフィルタ60によりとり出すことができる。

LCフィルタ60の代りにそれと同じ機能を果たす他の回路装置、たとえば、希望の2 KHz通過帯域を与えるように選択されたループ利得を有し、170 KHzでクロックされるCCD循環シフトレジスタを用いることができる。

以上説明した実施例はいろいろと変形して実施できる。たとえば、第3図の無安定回路の動作周波数を170 KHzから113 KHzに変え、単安定回路40により発生されるパルスの持続時間を短くして、小銃12が発射されるたびに113 KHzの1ミリ秒パルスパーストを2個レーザ装置36が発生できるようにすることがで

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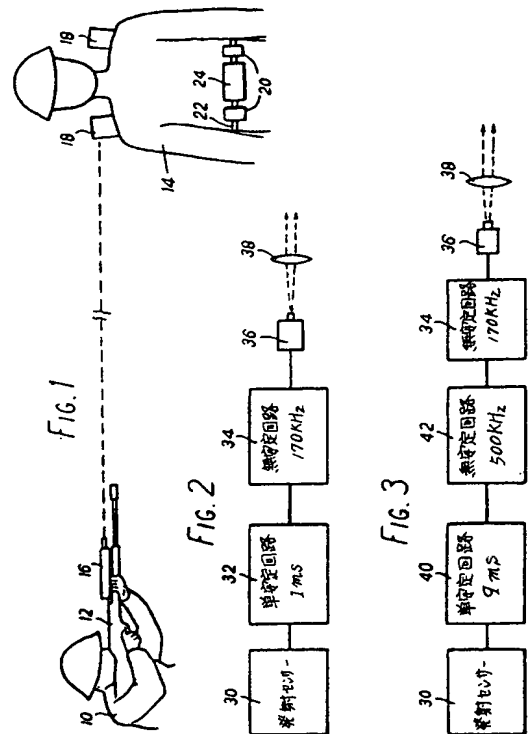
用い、「命中」(比較器74がトリガされる)と「外れ」(別の比較器はトリガされるが、比較器74はトリガされない)とを識別できるようにすることもできる。

比較的低出力のレーザ装置36と、1つの低雑音増幅器58へ並列に接続される無バイアスの検出器18, 20を用いることにより、シミュレータのそれぞれの部品の電力消費量を大幅に減少することができるが、それらの部品は通常は電池を電源としているから、消費電力の低減は非常に重要である。

きる。第4図に示されている検出器の回路、(1)帯域フィルタ60の各段をレーザのパルス繰り返し周波数の第4高調波すなわち452 KHzに同調させ、(2)それに対応して増幅器58の上限遮断周波数を高くし、(3)470 KHzに同調されている別の帯域フィルタを増幅器58の出力端子へ接続することにより変えた。それらのフィルタはともにセラミック・フィルタ素子を用いた。前記別のフィルタの出力は、第4図に示されているダイオード検波-復調器76と同じ検波-復調器と増幅度が3の増幅器を介して、比較器74の反転入力端子へ電圧 $V_B$ として加えられる。この比較器74の出力は二重パルス検出器、すなわち、所定の時間(たとえば1.5ミリ秒)以内での2個の連続パルスの発生を検出する検出器へと与えられる。この実施例の動作においては、広帯域ノイズすなわち衝撃性のノイズが2つのダイオード検波-復調器からほぼ等しい出力を生じさせるから、それらのノイズによつて比較器74はトリガされることはなく、したがつて二重パルス検出器の誤トリガは防止される。実際には、増幅度が3の増幅器により、ダイオード検波-復調器76の出力が他のダイオード検波復調器の出力より3倍以上大きい時だけ、比較器74をトリガできる。

希望によつては、比較器74に類似するが、ダイオード検波-復調器76からのより小さな振幅(すなわち低い相対振幅)のパルスによりトリガされる別の比較器を

浄書(内容に変更なし)



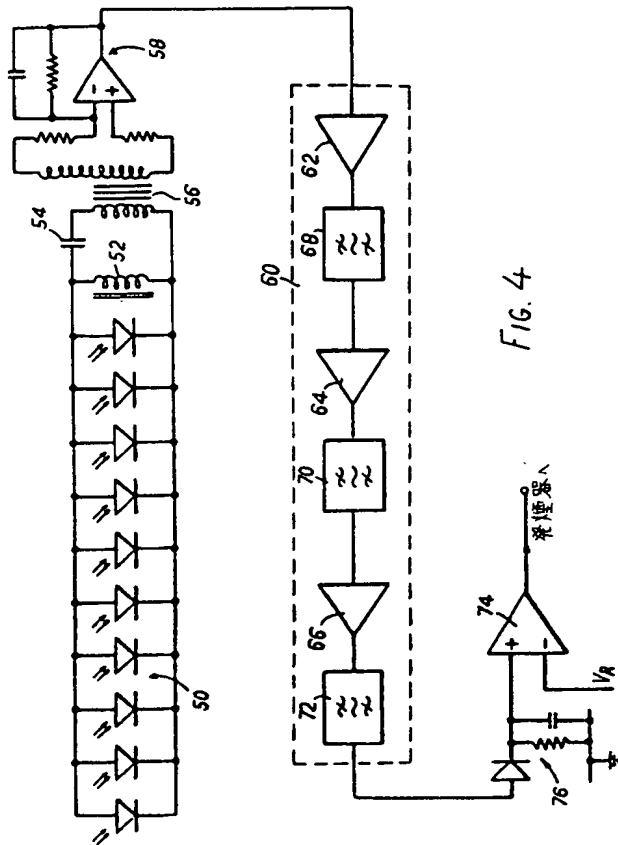


FIG. 4

手続補正書(方式)

昭和56年3月16日

特許庁長官 島田 春樹 殿

1. 事件の表示

昭和56年特許願第 PCT/GB 80/00092 号

2. 発明の名称

兵器効果シミュレータ

3. 補正をする者

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(電話東京(211)2321大代表)

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5. 補正命令の日付

昭和56年2月20日  
(発送日 昭和56年2月24日)

6. 補正により 補正の範囲

7. 補正の対象

図面の翻訳文

8. 補正の内容

図面の翻訳文の浄書(内容に変更なし)

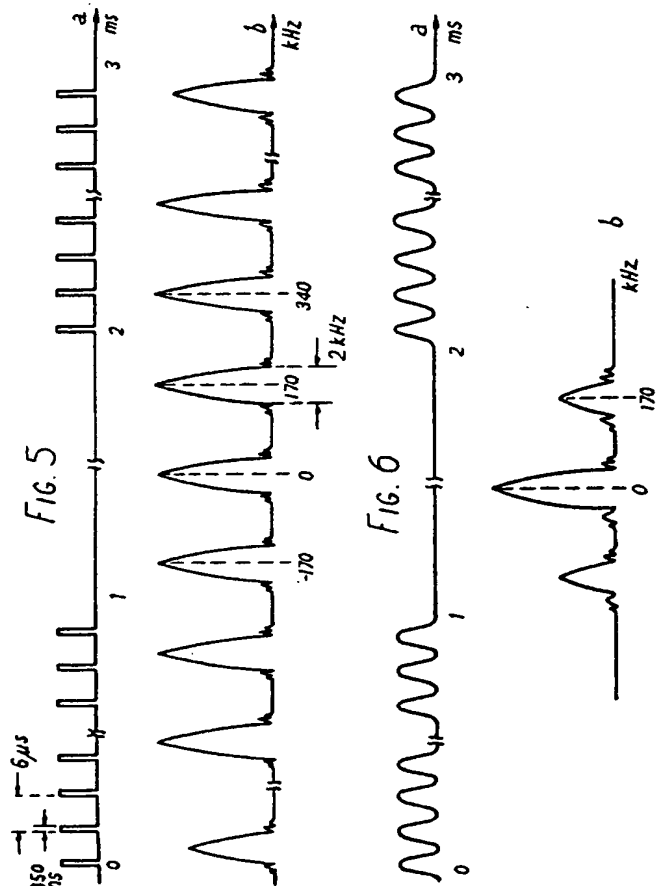


FIG. 5

FIG. 6

国際調査報告

International Application No. PCT/GB 80/00092

I. CLASSIFICATION OF SUBJECT MATTER (Of several classification symbols apply, indicate only 1)		
According to International Patent Classification (IPC) or to both National Classification and IPC		
Int.Cl. <sup>3</sup>	F 41 G 3/26	
II. FIELDS SEARCHED		
Minimum Documentation Searched		
Classification S. 210	Classification Symbols	
Int.Cl. <sup>3</sup>	F 41 G 3/26	
Documentation Searched other than Minimum Documentation		
In the extent that such Documents are included in the Fields Searched		
III. DOCUMENTS CONSIDERED TO BE RELEVANT <sup>1)</sup>		
Category <sup>2)</sup>	Copies of Documents, in such indication, where appropriate, of the relevant passages <sup>3)</sup>	Relevant to Claim No. 1
	GB, A, 1509562, published May 4, 1978 see figures 1-3; page 1, lines 50-64; page 2, lines 3-124, The Hetty Company	1,2
	US, A, 4054290, published October 18, 1977 see figure 1; column 2, lines 21-40, A.J. Villa	1,4
	US, A, 3104478, published September 24, 1963 see the whole document, L.W. Strauss et al.	1
	US, A, 3918714, published November 11, 1975 see figures 1,2; column 2, lines 29-61; column 3, lines 14-18, L. Ceccaroni	1,4
	US, A, 3257741, published June 28, 1966 see figure 1; from column 1, line 48, to column 3, line 23; column 4, lines 40-41, S.H. Cameron et al.	1,6
A	US, A, 3832791, published September 3, 1974 see the whole document, H.R. Robertsson	1
<sup>1)</sup> Special categories of cited documents: " A " document claiming the general state of the art " E " earlier document but published on or after the international filing date " L " document cited for special reason other than those referred to in the other categories " O " document referring to an oral disclosure, use, exhibition or other means " P " document published prior to the international filing date but on or after the priority date claimed " T " later document published on or after the international filing date or priority date and made in conflict with the application, but cited to understand the principle or theory underlying the invention " X " document of particular relevance <sup>2)</sup> Categories of documents: " A " document claiming the general state of the art " E " earlier document but published on or after the international filing date " L " document cited for special reason other than those referred to in the other categories " O " document referring to an oral disclosure, use, exhibition or other means " P " document published prior to the international filing date but on or after the priority date claimed " T " later document published on or after the international filing date or priority date and made in conflict with the application, but cited to understand the principle or theory underlying the invention " X " document of particular relevance <sup>3)</sup> Categories of documents: " A " document claiming the general state of the art " E " earlier document but published on or after the international filing date " L " document cited for special reason other than those referred to in the other categories " O " document referring to an oral disclosure, use, exhibition or other means " P " document published prior to the international filing date but on or after the priority date claimed " T " later document published on or after the international filing date or priority date and made in conflict with the application, but cited to understand the principle or theory underlying the invention " X " document of particular relevance		
IV. CERTIFICATION		
Date of the Actual Completion of the International Search	Date of Filing of the International Search Report	
29th July 1980	7th August 1980	
International Searching Authority	Signature of Authorized Officer	
European Patent Office	G.L.M. Krügerberg	

FURTHER INFORMATION CONTINUED FROM THE SECOND SHEET		
A	US, A, 3434226, published March 25, 1969 see the whole document, J.W. Schaller -----	1
<input type="checkbox"/> <b>OBSERVATIONS WHERE CERTAIN CLAIMS WERE FOUND UNSEARCHABLE <sup>10</sup></b> This international search report has not been established in respect of certain claims under Article 1700 (a) for the following reasons: 1. <input type="checkbox"/> Claim numbers _____, because they relate to subject matter <sup>11</sup> not required to be searched by this Authority, namely:   2. <input type="checkbox"/> Claim numbers _____, because they relate to parts of the international application that do not comply with the prescribed requirements to such an extent that no meaningful international search can be carried out <sup>12</sup> , specifically:   		
<input type="checkbox"/> <b>OBSERVATIONS WHERE UNITY OF INVENTION IS LACKING <sup>13</sup></b> This International Searching Authority found multiple inventions in this international application as follows:   1. <input type="checkbox"/> As all required additional search fees were timely paid by the applicant, this international search report covers all searchable claims of the international application. 2. <input type="checkbox"/> As only some of the required additional search fees were timely paid by the applicant, this international search report covers only those claims of the international application for which fees were paid, specifically claims:   3. <input type="checkbox"/> No required additional search fees were timely paid by the applicant. Consequently, this international search report is restricted to the invention first mentioned in the claims; it is covered by claim numbers:   Remark on Protest: <input type="checkbox"/> The additional search fees were accompanied by applicant's protest. <input type="checkbox"/> The protest accompanied the payment of additional search fees.		

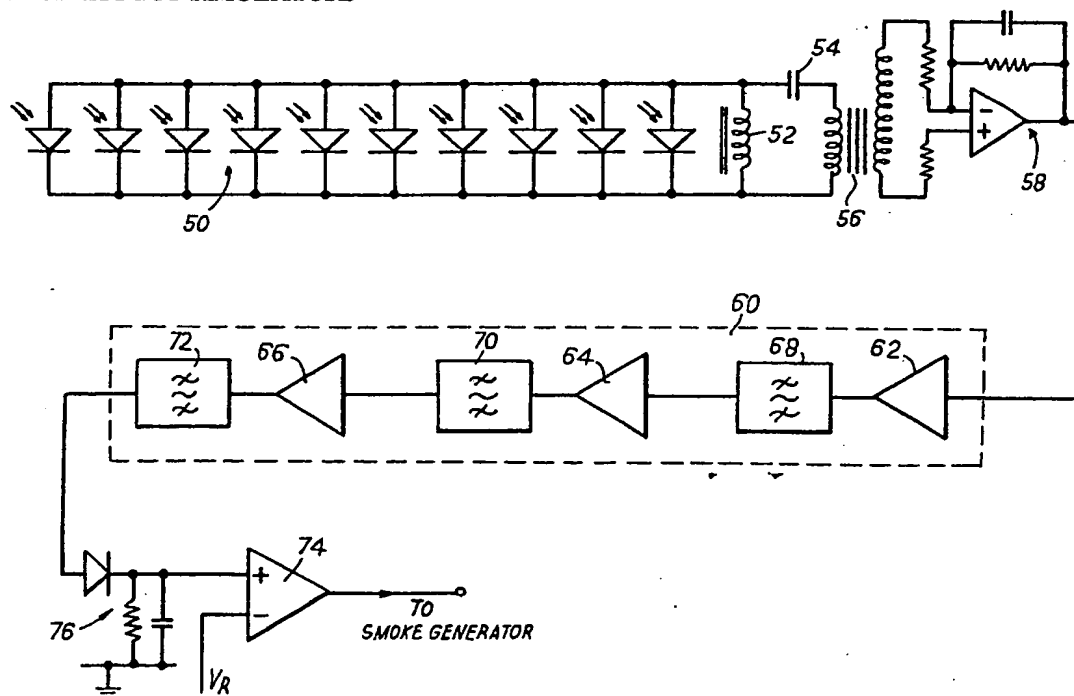
Form PCT/ISA 210 (Rev. 10-1979)



## INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification <sup>3</sup> :  F41G 3/26	A1	(11) International Publication Number: WO 80/02741  (43) International Publication Date: 11 December 1980 (11.12.80)
(21) International Application Number: PCT/GB 80/00092 (22) International Filing Date: 22 May 1980 (22.05.80) (31) Priority Application Number: 7918367 (32) Priority Date: 25 May 1979 (25.05.79) (33) Priority Country: GB  (71) Applicant (for all designated States except US): THE SOLARTRON ELECTRONIC GROUP LIMITED [GB/GB]; 124 Victoria Road, Farnborough, Hampshire GU14 7PW (GB). (72) Inventors; and (75) Inventors/Applicants (for US only): ASHFORD, David, William [GB/GB]; 27 St. Johns Road, Farnborough, Hampshire (GB). HUMMEL-NEWELL, Robert [GB/GB]; 6 Highfield Road, Cove, Farnborough, Hampshire (GB).		(74) Agents: COKER, David, G., et al.; Schlumberger Measurement and Control (UK) Limited, 124 Victoria Road, Farnborough, Hampshire GU14 7PW (GB).  (81) Designated States: DE, GB, JP, SE, US.  Published With international search report

(54) Title: WEAPON EFFECT SIMULATORS



## (57) Abstract

In a weapon effect simulator a low peak power laser projector (16) emits 1 milli-second bursts of radiation, each burst having either pulse or c.w. modulation at 170 kHz. A detector (18, 20, 24) for sensing the radiation has several photo-cells (50) connected in parallel to a single amplifier (58), and includes a bandpass filter (60) tuned to 170 kHz (chosen in harmonic relationship to the modulation frequency) and having a passband of 2kHz (inversely related to the duration of each radiation burst).



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WEAPON EFFECT SIMULATORSTECHNICAL FIELD

This invention relates to weapon effect simulators.

BACKGROUND ART

It is known to use a beam of electromagnetic radiation (typically from a laser) during simulated operation of a weapon for training purposes. In one type of system (UK Patent Specifications Nos. 1 228 143, 1 228 144, 1 439 612 and 1 451 192), the beam of radiation is pointed in the same direction as the weapon (for example, a gun) at the time of 'firing' the ammunition (a shell or bullet) with adjustment for such factors as aim-off if appropriate. In another type (UK Patent Specifications Nos. 1 300 941 and 1 300 942) the beam is pointed to intersect continuously the path that the ammunition (for example, a missile) would follow in a live firing. In either case, the result is that the beam of radiation is directed at the point in space occupied by the ammunition when it reaches the vicinity of the target.

Such systems basically involve a device, commonly known as a projector, for generating, and if necessary orienting, the beam of radiation, and another device, known as a detector, for detecting incidence of the radiation on the target. The detector may be mounted on the target itself, or it may be associated with the projector, the radiation being reflected from the target by a retro-reflector mounted thereon.

In known systems, the projector has been arranged to generate radiation in the form of pulses of very short duration and relatively high peak power. Consequently, the detector (a photo-cell coupled to an amplifier) has been designed essentially to detect each pulse of radiation as an individual, discrete entity. Because of the abrupt nature of the pulses, the bandwidth of the detector amplifier has to



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be relatively large to ensure reliable detection of a pulse, which in turn limits to one the number of photo-cells which can be connected to an amplifier if an acceptable signal-to-noise ratio is to be maintained. In practice, a target needs to be fitted with at least four photo-cells to ensure detection of radiation from any direction around the target, and each of these photo-cells requires its own sensitive, stable, wide-bandwidth (and therefore expensive) amplifier.

#### DISCLOSURE OF INVENTION

According to one aspect of this invention there is provided a weapon effect simulator having a projector arranged to project a beam of electromagnetic radiation during simulated firing of a weapon and a detector arranged to detect incidence of said radiation thereupon, wherein:

said projector is arranged to generate at least one burst of radiation for each said firing, said burst being of predetermined duration and being modulated at a predetermined frequency;

and

said detector includes frequency-selective means tuned to a frequency harmonically related to said predetermined frequency and having a pass band dependent upon said predetermined duration.

The radiation is detected by detection of the overall burst and its modulation (which can, for example, be pulse modulation or continuous-wave modulation), rather than by separate detection of individual pulses (in the case of pulse modulation). The frequency-selective means is conveniently tuned to said predetermined frequency.

The pass band of the frequency-selective means may be substantially equal to twice the reciprocal of said predetermined duration. By making this duration relatively long (for example, one millisecond), the pass band can be made very narrow (only 2 kHz), thereby diminishing noise considerably, to the extent that several photo-cells can be coupled in parallel. Furthermore the peak power that must be



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radiated for a given signal-to-noise ratio is substantially reduced, permitting the use, for example, of low peak power, higher mean power devices such as double heterostructure lasers and small source light emitting diodes.

#### BRIEF DESCRIPTION OF DRAWINGS.

A weapon effect simulator in accordance with this invention will now be described, by way of example, with reference to the accompanying drawings, in which:-

Figure 1 depicts an attacking soldier and a target soldier;

Figure 2 is a block schematic diagram of one form of projector;

Figure 3 is a block schematic diagram of another form of projector;

Figure 4 is a circuit diagram of a detector;  
and

Figures 5 and 6 are waveform and spectral diagrams illustrating pulse modulation and continuous-wave modulation respectively.

#### BEST MODE FOR CARRYING OUT THE INVENTION/INDUSTRIAL APPLICABILITY

Referring to Figure 1, an attacking soldier 10 under training is aiming a rifle 12 at a target soldier 14. The rifle 12 is loaded with blank ammunition and carries a laser projector 16. The target soldier 14 has two detectors 18 on his shoulders and four more detectors 20 on a belt 22 about his waist. All the detectors 18 and 20 are connected to a control unit and smoke generator 24 also carried on the belt 22.

When the soldier 10 pulls the trigger of the rifle 12, the blank ammunition is fired, giving appropriate aural and visual effects. At the same time, the laser projector 16 is automatically operated to project a beam of electromagnetic radiation along the direction of aim of the rifle 12. If the rifle 12 has been accurately aimed at the soldier 14, the radiation will strike the detectors 18 and/or 20, causing a signal to be sent to the control unit 24 which thereupon releases smoke to indicate that the target soldier 14 has been 'hit'. If the target soldier 14 has a rifle, this can be coupled to the control unit 24 to be inhibited



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from 'firing' in the event of a 'hit'.

The design and operation of the projector 16 and the control unit 24 will now be described in more detail with reference to Figures 2 to 6.

Referring to Figure 2, the firing of the rifle 12 is detected by a firing sensor 30, which may be, for example, a microphone and amplifier to detect the sound of the rifle 12 being fired, or a pressure-responsive switch operated by the back pressure in the rifle barrel when the blank ammunition is fired. The sensor 30 triggers a monostable circuit 32 which supplies a pulse of 1 millisecond duration to enable an astable circuit 34. This astable circuit 34 supplies pulses at a repetition frequency of 170 kHz to a gallium arsenide double-heterostructure laser device 36, to generate pulses of infra-red radiation at a rate of 170 kHz for 1 millisecond. A lens in front of the laser device 36 focusses the radiation into a beam.

In the projector illustrated in Figure 2, only a single burst of pulses of radiation is emitted each time the rifle 12 is fired. However, if desired, several bursts may be emitted for each firing, using the circuit shown in Figure 3.

Referring to Figure 3, the firing sensor 30 is coupled to the astable circuit 34 via a monostable circuit 40 and a second astable circuit 42. The monostable circuit 40, when triggered, supplies a pulse having a duration of 9 milliseconds, thereby enabling the astable circuit 42 which runs at a frequency of 500 Hz. Thus the astable circuit 34 is in turn enabled for five periods each 1 millisecond in duration and spaced 1 millisecond apart, and the laser device 36 emits five corresponding bursts of 170 kHz pulses of infra-red radiation.

Referring now to Figure 4, the detectors 18, 20 are



represented by ten unbiassed photo-sensitive silicon cells 50 connected in parallel with each other and with a choke 52. The choke 52 provides a d.c. leakage path for charge induced in the cells 50 by ambient light, thereby preventing such charges from accumulating and saturating the cells 50. High-frequency signals, which are not affected by the choke 52, are coupled by a capacitor 54 to a primary winding of a coupling transformer 56. The turns ratio of this transformer 56 is selected for optimum signal-to-noise ratio, and the secondary winding of the transformer feeds a low-noise amplifier 58 of conventional design, having a low-value feedback capacitor to limit its high-frequency response.

The output of the amplifier 58 is coupled to a three-stage bandpass filter 60, each stage of which comprises an amplifier 62, 64, 66 and an associated parallel-resonant bandpass LC filter 68, 70, 72 tuned to 170 kHz and having a passband of 2 kHz. The filtered signal is then supplied to a comparator 74, which controls the smoke generator, via a diode detector-demodulator 76.

In use, pulses of infra-red radiation incident upon any of the detectors 18, 20 (that is, on any of the photo-cells 50) cause corresponding electrical pulses to be supplied via the capacitor 54 and the transformer 56 to the amplifier 58. After amplification, the 1 millisecond bursts of 170 kHz pulses are selectively passed by the filter 60 to the comparator 74 which actuates the smoke generator if the amplitude of the filtered signal exceeds a threshold voltage  $V_R$ .

Figure 5 (a) shows the waveform of typical bursts of infra-red radiation, each comprising pulses 350 nanoseconds long repeated at intervals of 6 microseconds for a period of 1 millisecond. The frequency-domain equivalent of this waveform is shown in Figure 5 (b), and comprises a main lobe centred on 0 Hz and additional lobes centred on integral multiples of 170 kHz, each lobe embracing a frequency range of 2 kHz.



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The effect of the filter 60 is to select the lobes centred on + 170 kHz and - 170 kHz (where the negative sign indicates a signal in anti-phase to one having a positive sign). The 2 kHz passband of the filter 60 is related to the 2 kHz range of the lobes in the frequency spectrum of the pulse bursts, and this range is in turn determined (on an inverse basis) by the 1 millisecond duration of each burst. The operation of the filter can thus be considered as being the integration of all the pulses of a burst for the duration of the burst, so the energy associated with each individual pulse is aggregated with that of all the other pulses in the burst. Consequently, a laser device which is capable of relatively high mean power but relatively low peak power, such as the (relatively cheap) double heterostructure device mentioned previously, can be used in the projector 16. This in turn confers advantages in terms of stability of operation of the projector with change in temperature, and permits the use of small, low-voltage drive transistors with the laser device. The relatively narrow (2 kHz) bandwidth of the filter 60 also significantly limits the proportion of the noise signal from the photo-cells 50 which can reach the comparator 74, thereby facilitating the use of a low peak power laser device and permitting the parallel connection of several photo-cells 50 to a single amplifier 58 as shown in Figure 4.

Using the bandpass filter 60 tuned to 170 kHz instead of a low pass filter (to detect the main lobe centred on 0 Hz - Figure 5b), avoids spurious output signals arising either from sudden changes in ambient light or from artificial light sources to which the apparatus may be exposed during fitting and setting up. The bandpass filter 60 could be tuned to a harmonic of the pulse repetition frequency (such as 340 kHz) rather than to the repetition frequency of 170 kHz itself. Furthermore, the frequency selection could be performed before the coupling transformer 56, by selecting the inductance of the choke 52 to resonate with the combined self-capacitance of the photo-cells 50 at the desired bandpass frequency.

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Instead of pulse modulation of the radiation emitted by the projector 16, it is also possible to use continuous-wave modulation, as illustrated in Figure 6 (a). In this case, the astable circuit 34 of Figures 2 and 3 would be replaced by a suitable sine-wave oscillator. Figure 6 (b) shows the frequency spectrum of this type of modulation, for which the bandpass filter 60 would be tuned to the modulation frequency (170 kHz) of the 1-millisecond bursts of radiation. With c.w. modulation, for which a striped-geometry type of laser or small source light emitting diode is particularly suitable, rather more of the modulation power (up to half) can be extracted by the filter 60 than is the case with pulse modulation.

The LC filter 60 could be replaced by other circuitry having the same function, such as a CCD recirculating shift register clocked at 170 kHz and having a loop gain chosen to provide the desired 2 kHz passband.

Various other modifications can be made to the described embodiment of the invention. For example, in another embodiment of the invention, the operating frequency of the astable circuit of Figure 3 was changed from 170 kHz to 113 kHz, and the duration of the pulse produced by the monostable circuit 40 was reduced so that the laser device 36 produced two 1 millisecond bursts of 113 kHz pulses of infra-red radiation for each firing of the rifle 12. The detector circuitry of Figure 4 was also modified, by (i) tuning each stage of the bandpass filter 60 to the fourth harmonic of the laser p.r.f, that is to 452 kHz, (ii) correspondingly increasing the upper cut off frequency of the amplifier 58, and (iii) connecting a further bandpass filter, tuned to 470 kHz, to the output of the amplifier 58: both bandpass filters used ceramic filter elements. The output of this further filter was applied, via a diode detector-demodulator identical to that shown at 76 in Figure 4 and a x3 amplifier, to the inverting input of the comparator 74 (i.e. as the voltage  $V_P$ ). The output of the comparator 74 was then connected to a double-pulse detector, ie a detector which





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detects the occurrence of two consecutive pulses within a predetermined time period, eg  $1\frac{1}{2}$  milliseconds. In operation of this embodiment, wide-band or impulsive noise tended to produce substantially equal outputs from both the diode detector-demodulators, so the comparator 74 was not triggered by such noise and spurious triggering of the double-pulse detector was prevented. In fact, the x3 amplifier ensures that the comparator 74 can be triggered only when the signal appearing at the output of the diode detector-demodulator 76 exceeds that at the output of the other diode detector-demodulator by more than a factor of three.

If desired, a further comparator similar to the comparator 74, but triggered by pulses of lower amplitude (or lower relative amplitude) from the diode detector-demodulator 76, can be provided, in order to permit a distinction to be made between a "hit" (comparator 74 triggered) and a "near miss" (further comparator triggered, but comparator 74 not triggered).

The use of the relatively low-powered laser device 36, and the use of the unbiased detectors 18, 20 connected in parallel to the single low-noise amplifier 58, each help to significantly reduce the power consumption of their respective parts of the simulator, which, since these parts are normally battery-powered, is very important.

CLAIMS

1. A weapon effect simulator having a projector arranged to project a beam of electromagnetic radiation during simulated firing of a weapon and a detector arranged to detect incidence of said radiation thereupon, characterised in that:  
said projector is arranged to generate at least one burst of radiation for each said firing, said burst being of predetermined duration and being modulated at a predetermined frequency;  
and in that  
said detector includes frequency-selective means tuned to a frequency harmonically related to said predetermined frequency and having a pass band dependent upon said predetermined duration.
2. A simulator according to claim 1, wherein said modulation is pulse modulation.
3. A simulator according to claim 1, wherein said modulation is continuous-wave modulation.
4. A simulator according to claim 1, wherein said frequency-selective means is tuned to said predetermined frequency.
5. A simulator according to claim 1, wherein said pass band is substantially equal to twice the reciprocal of said predetermined duration.
6. A simulator according to claim 1, wherein said detector has a plurality of light-sensitive cells coupled in parallel to a single amplifier.



FIG. 1

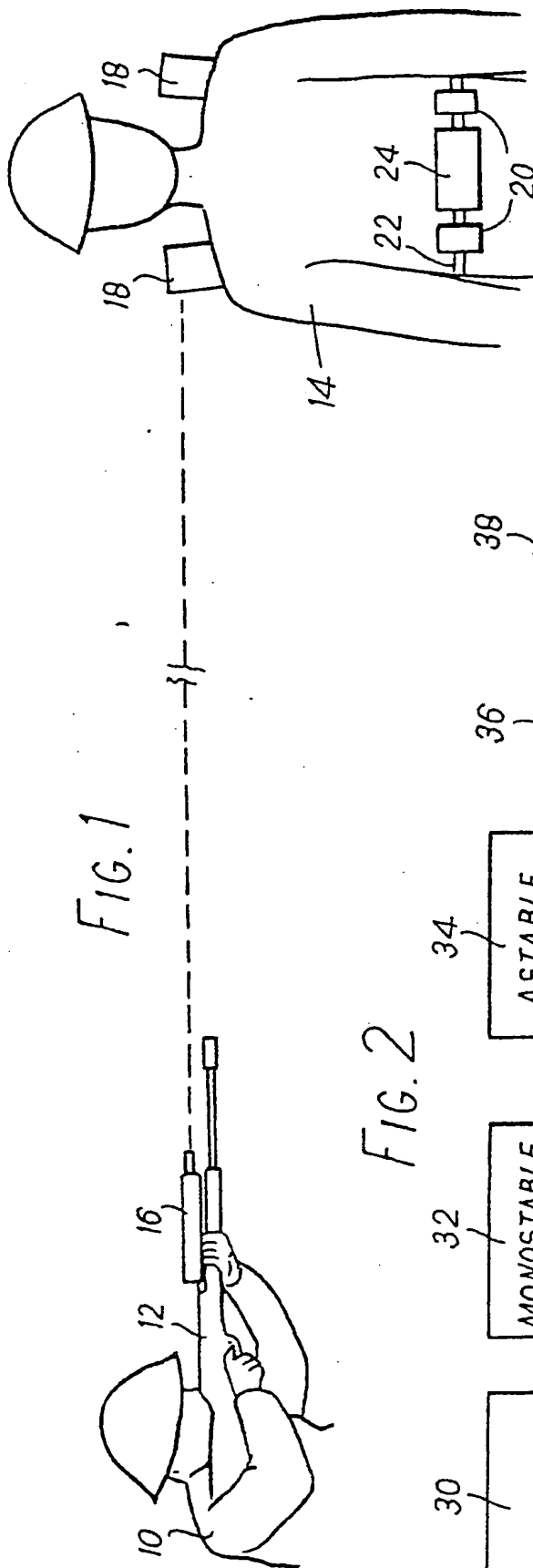


FIG. 2

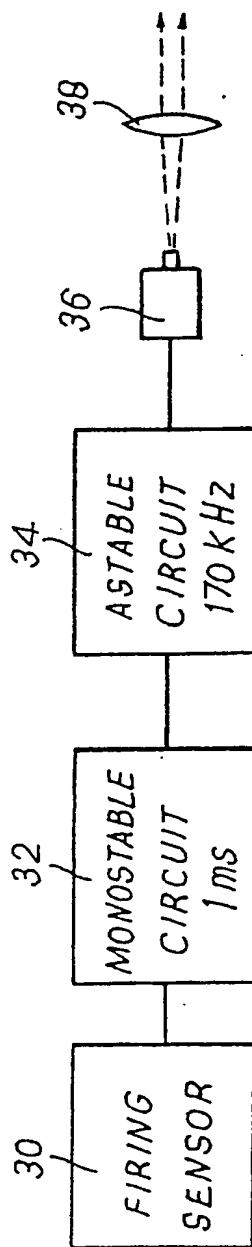
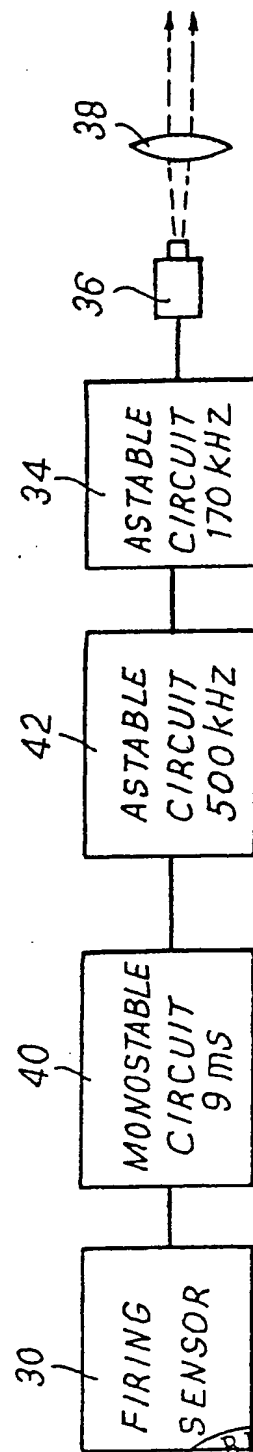


FIG. 3



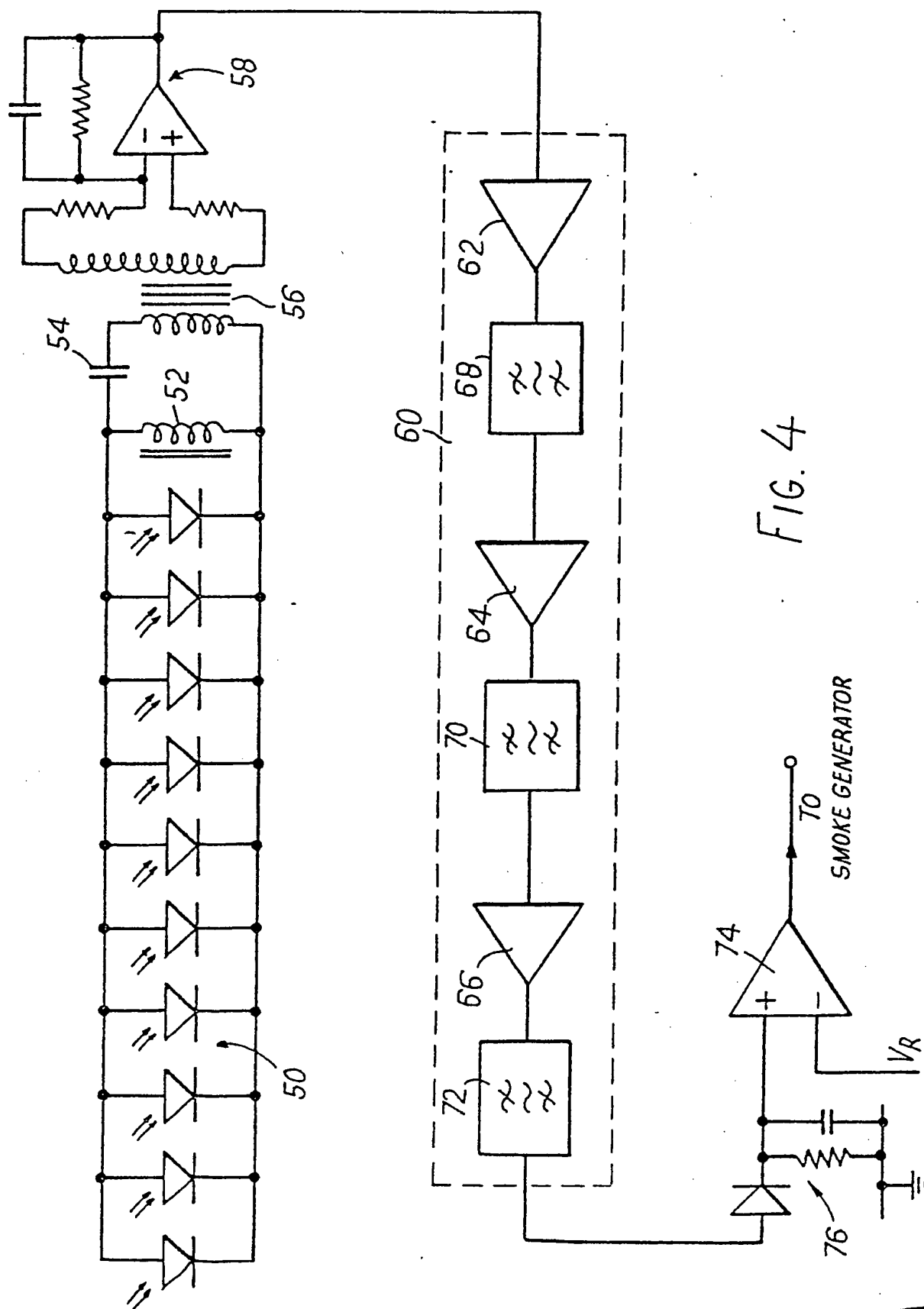
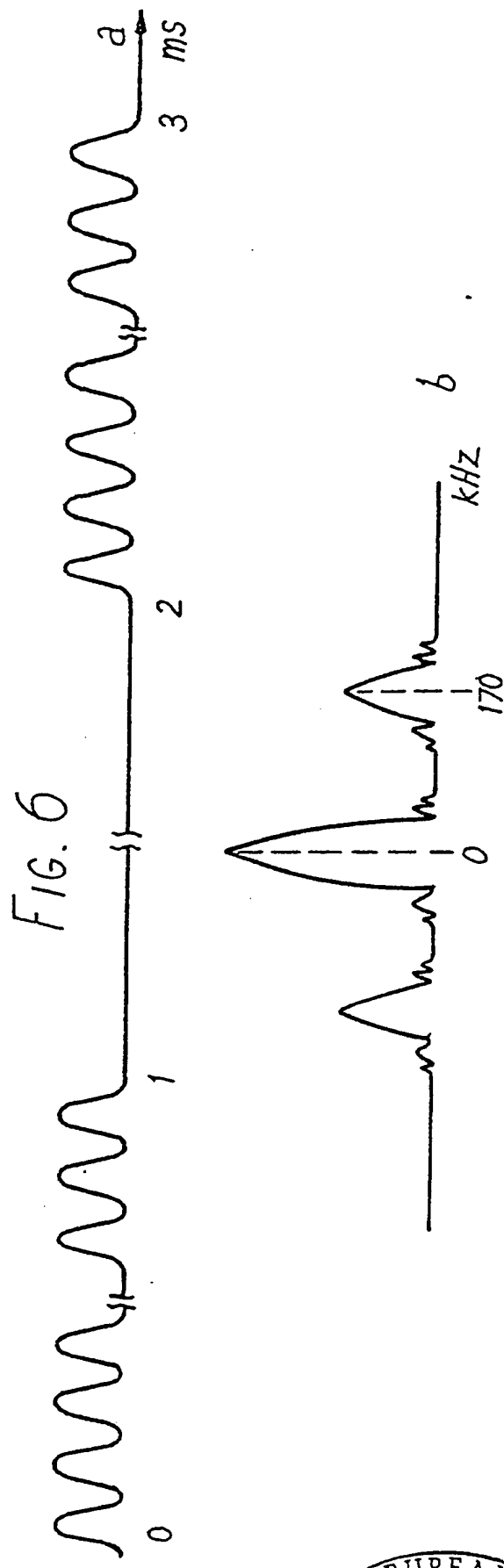
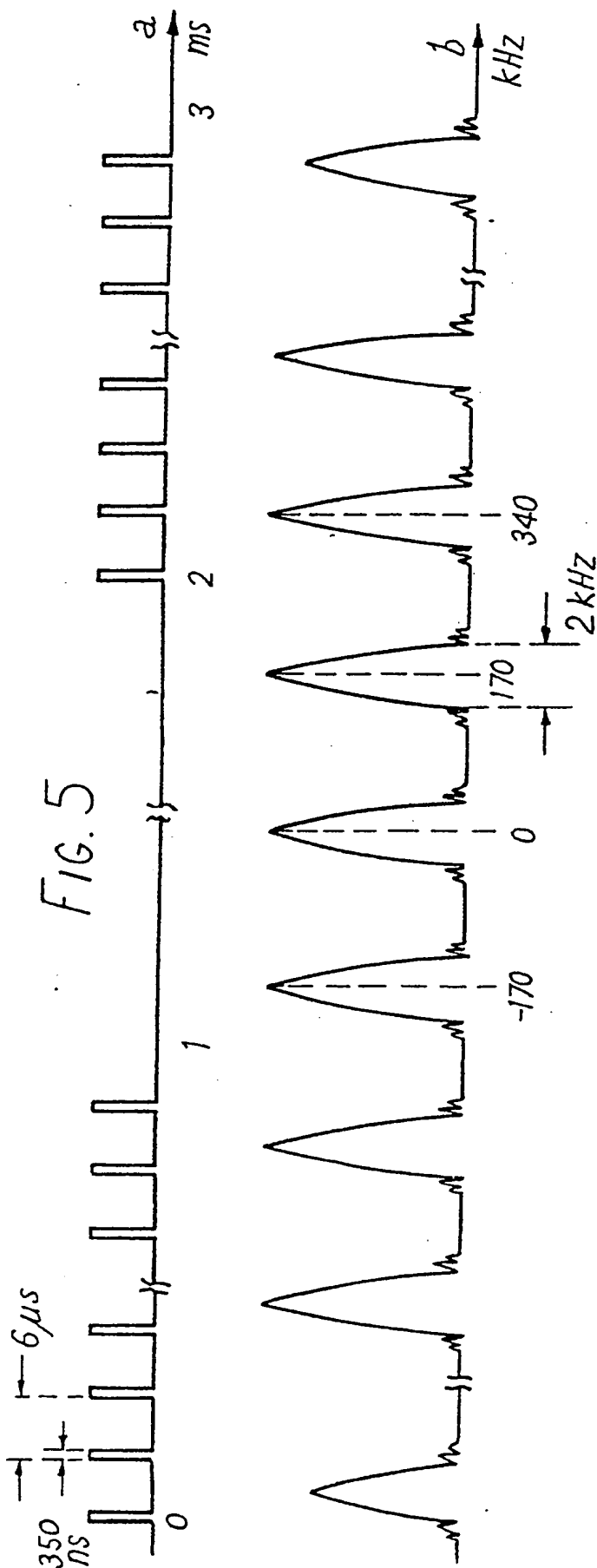


FIG. 4



## I. CLASSIFICATION OF SUBJECT MATTER (if several classification symbols apply, indicate all) \*

According to International Patent Classification (IPC) or to both National Classification and IPC

Int.Cl.<sup>3</sup> F 41 G 3/26

## II. FIELDS SEARCHED

Minimum Documentation Searched \*

Classification System

Classification Symbols

Int.Cl.<sup>3</sup> F 41 G 3/26Documentation Searched other than Minimum Documentation  
to the extent that such Documents are included in the Fields Searched \*III. DOCUMENTS CONSIDERED TO BE RELEVANT <sup>14</sup>

Category *	Citation of Document, <sup>16</sup> with indication, where appropriate, of the relevant passages <sup>17</sup>	Relevant to Claim No. <sup>14</sup>
	GB, A, 1509562, published May 4, 1978 see figures 1-3; page 1, lines 50-64; page 2, lines 3-124, The Mettoy Company --	1,2
	US, A, 4054290, published October 18, 1977 see figure 1; column 2, lines 21-40, A.J. Villa --	1,4
	US, A, 3104478, published September 24, 1963 see the whole document, L.W. Strauss et al. --	1
	US, A, 3918714, published November 11, 1975 see figures 1,2; column 2, lines 29-61; column 3, lines 14-18, L. Ceccaroni --	1,4
	US, A, 3257741, published June 28, 1966 see figure 1; from column 1, line 48, to column 3, line 23; column 4, lines 40-41, S.H. Cameron et al. --	1,6
A	US, A, 3832791, published September 3, 1974 see the whole document, H.R. Robertsson --	1 ./.

\* Special categories of cited documents: <sup>15</sup>

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date or priority date and not in conflict with the application,  
but cited to understand the principle or theory underlying  
the invention

"X" document of particular relevance

## IV. CERTIFICATION

Date of the Actual Completion of the International Search \*

29th July 1980

Date of Mailing of this International Search Report \*

7th August 1980

International Searching Authority \*

European Patent Office

Signature of Authorized Officer <sup>18</sup>

G.L.M. Kruidenberg

A US, A, 3434226, published March 25, 1969  
see the whole document, J.W. Schaller  
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1

V. ☐ OBSERVATIONS WHERE CERTAIN CLAIMS WERE FOUND UNSEARCHABLE <sup>10</sup>

This International search report has not been established in respect of certain claims under Article 17(2) (a) for the following reasons:

1. ☐ Claim numbers \_\_\_\_\_, because they relate to subject matter <sup>12</sup> not required to be searched by this Authority, namely:
2. ☐ Claim numbers \_\_\_\_\_, because they relate to parts of the International application that do not comply with the prescribed requirements to such an extent that no meaningful international search can be carried out <sup>13</sup>, specifically:

VI. ☐ OBSERVATIONS WHERE UNITY OF INVENTION IS LACKING <sup>11</sup>

This International Searching Authority found multiple inventions in this International application as follows:

1. ☐ As all required additional search fees were timely paid by the applicant, this International search report covers all searchable claims of the International application.
2. ☐ As only some of the required additional search fees were timely paid by the applicant, this international search report covers only those claims of the international application for which fees were paid, specifically claims:
3. ☐ No required additional search fees were timely paid by the applicant. Consequently, this international search report is restricted to the invention first mentioned in the claims; it is covered by claim numbers:

## Remark on Protest

- ☐ The additional search fees were accompanied by applicant's protest.
- ☐ No protest accompanied the payment of additional search fees.